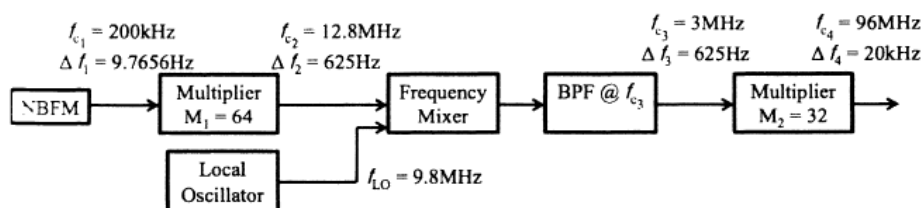


## Solutions to Homework #8

1. [10 points](L&D Exercise 5.3-1) Design (the block diagram of) an Armstrong indirect FM modulator to generate an FM carrier with a carrier frequency of 96 MHz and  $\Delta f = 20$  kHz. A narrowband FM generator with  $f_c = 200$  kHz and adjustable  $\Delta f$  in the range of 9 to 10 Hz is available. The stockroom also has an oscillator with adjustable frequency in the range of 9 to 10 MHz. There are bandpass filters with any center frequency, and only frequency doublers are available.

**Solutions:** The design is shown in the figure below.



In this case, the NBFM generator generates  $f_{c1} = 200 \text{ kHz}$  and  $\Delta f_1 = 9$  to  $10 \text{ Hz}$ . The final WBFM should have  $f_{c4} = 96 \text{ MHz}$  and  $\Delta f_4 = 20 \text{ kHz}$ . The total factor of frequency multiplication needed is  $M_1 \cdot M_2 = \frac{\Delta f_4}{\Delta f_1} = 2000$  to  $2222$ . Because only frequency doublers are available, we find that  $M_1 \cdot M_2 = 2^{11}$ , and  $\Delta f_1 = \frac{\Delta f_4}{2^{11}} = 9.7656 \text{ Hz}$ .

Now, let  $M_1 = 2^{n_1}$ ,  $M_2 = 2^{n_2}$ ,  $n_1 + n_2 = 11$ ,  $f_{c2} = 2^{n_1} f_{c1}$ , and  $f_{c4} = 2^{n_2} f_{c3}$ . In order to find  $f_{LO}$ , there are three possible relationships:  $f_{c3} = f_{c2} \pm f_{LO}$  and  $f_{LO} - f_{c2}$ . Each should be tested to determine the one that will require  $9^6 \leq f_{LO} \leq 10^7$ .

First, we test  $f_{c3} = f_{c2} - f_{LO}$ . This case leads to

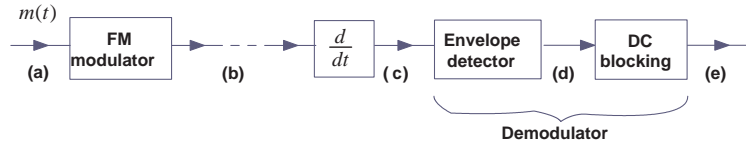
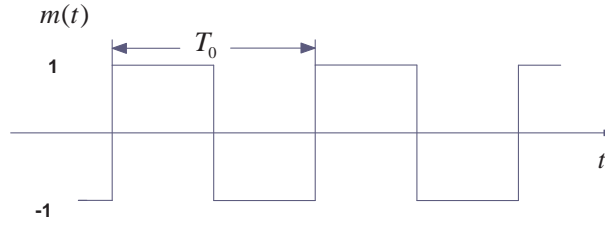
$$96 \text{ MHz} = f_{c4} = 2^{n_2} f_{c3} = 2^{n_2} (f_{c2} - f_{LO}) = 2^{n_2} (2^{n_1} f_{c1} - f_{LO}) = 2^{11} (200 \times 10^3) - 2^{n_2} f_{LO}.$$

Thus, we have

$$f_{LO} = 2^{-n_2} (4.096 \times 10^8 - 9.6 \times 10^7) = 2^{-n_2} (3.136 \times 10^8).$$

In this case, if  $n_2 = 5$  then  $f_{LO} = 9.8 \text{ MHz}$ , which is in the desired range. We will not test the other cases since this one works. Thus, the final design is  $M_1 = 2^6 = 64$ ,  $M_2 = 32$ , and  $f_{LO} = 9.8 \text{ MHz}$ . This gives  $f_{c2} = 2^{n_1} f_{c1} = 12.8 \text{ MHz}$ ,  $\Delta f_2 = M_1 \times \Delta f_1 = 625 \text{ Hz}$ ,  $f_{c3} = f_{c2} - f_{LO} = 12.8 - 9.8 = 3 \text{ MHz}$ ,  $\Delta f_3 = 625 \text{ Hz}$ . The bandpass filter used will be centered at 3 MHz.

2. [10 points] (L&D Exercise 5.4-2) A periodic square wave  $m(t)$  (shown in the figure below) frequency-modulates a carrier of frequency  $f_c = 10$  kHz with  $\Delta f = 1$  kHz. The carrier amplitude is  $A$ . The resulting FM signal is demodulated, as also shown in the figure below. Sketch the waveforms at points  $b, c, d$ , and  $e$ . (Note that the DC blocking in the following figure suppresses the none time-varying part of the signal.)



**Solutions:** Given that  $f_c = 10$  kHz,  $\Delta f = 1$  kHz, and that the message is periodic square wave of period  $T_0$ , the resulting FM signal has instantaneous frequency  $f_i = f_c \pm \Delta f$ , which switches from 11 kHz to 9 kHz and back over one period. Thus,

$$\varphi_{FM}(t) = A \cos[20000\pi t \pm 2000\pi t]$$

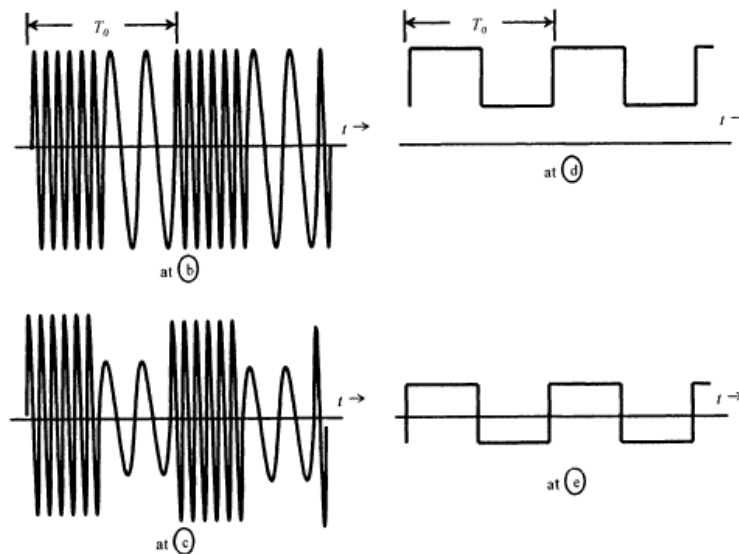
over any given half period. This signal is shown in the figure below as (b).

Now, after the ideal differentiator,

$$\dot{\varphi}_{FM}(t) = -(20000\pi \pm 2000\pi)A \sin[20000\pi t \pm 2000\pi t]$$

This signal is shown in the figure below as (c). Comparing with (b), this signal also has its amplitude switching between  $22000\pi A$  and  $18000\pi A$ .

Next, after the envelope detector, the output will be a periodic square wave proportional to  $(20000\pi \pm 2000\pi)A$ , with a DC offset as shown in the figure below as (d). After DC blocking, the DC constant  $20000\pi$  is removed, and the result is a periodic square wave proportional to  $m(t)$ . This is illustrated in the figure below as (e).



3. [10 points] (L&D Exercise 5.4-3) Let  $s(t)$  be an angle-modulated signal that a receiver obtains,

$$s(t) = 2 \cos [10^7 \pi t + 2 \sin(2000\pi t + 0.3\pi) - 3\pi \cos(100t)] .$$

- (a) Find the bandwidth of this FM signal.
- (b) If  $s(t)$  is sent to an (ideal) envelope detector, find the detector output signal.
- (c) If  $s(t)$  is first differentiated before the envelope detector, find the detector output signal.
- (d) Explain which detector output can be processed to yield the message signal  $m(t)$  and find the message signal  $m(t)$  if  $k_f = 200\pi$ .

**Solutions:**

(a) From the form of  $s(t)$ , we know that

$$k_f \int_0^t m(\alpha) d\alpha = 2 \sin(2000\pi t + 0.3\pi) - 3\pi \cos(100t),$$

Taking derivative of the above equation, we have

$$k_f m(t) = 4000\pi \cos(2000\pi t + 0.3\pi) + 300\pi \sin(100t),$$

It is clear that the bandwidth of  $m(t)$  is  $B = 1\text{kHz}$ . From the above equation, we also have  $k_f m_p = 4300\pi$  and  $\Delta f = \frac{k_f m_p}{2\pi} = 2150\text{Hz}$ . Therefore,  $B_{FM} = 2(\Delta f + B) = 6.3\text{kHz}$ .

(b) The envelope of  $s(t)$  is 2.

(c) Taking derivative of  $s(t)$  with respect to  $t$ , we get

$$\dot{s}(t) = -2(10^7 \pi + 4000\pi \cos(2000\pi t + 0.3\pi) + 300\pi \sin(100t)) \sin(10^7 \pi t + 2 \sin(2000\pi t + 0.3\pi) - 3\pi \cos(100t)),$$

so the envelope detector output is

$$2(10^7 \pi + 4000\pi \cos(2000\pi t + 0.3\pi) + 300\pi \sin(100t)).$$

(d) The envelope in (c) can be processed to yield the message signal  $m(t)$ . Passing the envelope of  $\dot{s}(t)$  through a DC blocking, the signal becomes  $8000\pi \cos(2000\pi t + 0.3\pi) + 600\pi \sin(100t)$ , which is  $2k_f m(t)$ . We then pass this signal through an amplifier with gain  $\frac{1}{2k_f} = \frac{1}{400\pi}$  to obtain the output  $m(t)$ .